

Method and Device for determining wheel force

The present invention relates to a method and a device for determining wheel force exerted on a vehicle wheel during running.

In recent years, the number of vehicles equipped with computer-aided control systems such as anti-lock brake system, attitude control system (suspension control system) and steer-by-wire system is rising.

In such control systems, if data on the magnitude and direction of the wheel force exerted on a rolling vehicle wheel can be utilized, control accuracy will be dramatically improved. Hitherto, however, there is no way to get data on the wheel forces exerted on rolling vehicle wheels during running. In the car industry, therefore, there is a great demand for a device which can monitor the forces exerted on vehicle wheels during running.

It is therefore, an object of the present invention to provide a method and device by which a force exerted on a vehicle wheel during running can be easily determined.

According to one aspect of the present invention, a method for determining force exerted on a vehicle wheel comprises:

obtaining data on functionality between the force exerted on a vehicle wheel and a physical parameter of a radius part of the vehicle wheel at at least one predetermined measuring position;

making a formula of the physical parameter for the force, using the obtained data on the functionality;

measuring the physical parameter of the vehicle wheel

during rolling; and

computing the formula using the measured physical parameter to work out the force.

According to another aspect of the present invention, a device for determining force exerted on a vehicle wheel comprises:

at least one sensor for a physical parameter of the vehicle wheel,

a memory on which data on functionality between the force and physical parameter are stored,

a processor which, using data on the physical parameter read from said at least one sensor and the stored data on functionality, works out the force and outputs data on the force.

Embodiments of the present invention will now be described in detail in conjunction with the accompanying drawings.

Fig.1 is a schematic side view of a vehicle wheel.

Fig.2 is a diagram for explaining functionality or relationships between variations of strain and wheel forces exerted on a vehicle wheel.

Fig.3 is a diagram showing the physical relationship between the vehicle wheel and a xyz orthogonal coordinate system and the measuring positions P1-P4 on the wheel plane.

Fig.4 is a diagram showing a system of determining wheel force according to the present invention.

Fig.5 is a flowchart for determining wheel forces on each wheel in the system shown in Fig.4.

Figs.6 and 7 each shows an example of the arrangement of sensors for locating the sensors.

The gist of the present invention is to determine at least one kind of forces exerted on a vehicle wheel by utilizing a variation of a physical parameter of the rolling vehicle wheel itself.

Here, a vehicle wheel 2 comprises an radially outermost annular part 2a contacting with the road surface to cause friction against the road surface, and a radius part 2b2 extending radially outwardly from a hub attached to a vehicle axle towards the annular part 2a. In case of automobile, as shown in Fig.1, a vehicle wheel 2 generally comprises a tire 2a and a wheel 2b. The tire 2a may be not only a pneumatic tire but also solid tire or the like. The wheel 2b comprises a rim 2b1 on which the tire is mounted and a wheel disk 2b2 between the rim and a hub attached to a vehicle axle. The wheel disk 2b2 is the above-mentioned radius part, and thus it is meant for not only a disk-like relatively thin part but also radius rods, spokes and the like.

As to the physical parameter, a strain is used in the following embodiment. But other parameters such as stress, magnetic property and optical property may be used too. More specifically, in the following embodiment, the strain in the radial direction measured at a position on the wheel disk 2b2 is used. But, it may be possible to use another direction and another position.

Fig.2 shows exemplary variations of strain of a vehicle wheel which is rolling under the following conditions (1), (2), (3) and (4) where various forces F are exerted on the wheel axis CL.

Condition	line	Wheel force F			
		Vertical force Fx(kgf)	Lateral force Fy(kgf)	Longitudinal force (kgf)	Torque Fx(kgf·m) around x-axis
1)	continuous line	500	0	0	0
2)	dashed line	500	400	0	0
3)	broken line	500	0	400	0
4)	double-dashed line	500	0	0	5

The strain was measured at a fixed position on the wheel disk (radius part) $2b^2$ as a tensile strain (-) or compressive strain (+) in the radial direction.

The test tire used was a pneumatic radial tire of size 195/60R15 for passenger cars. The wheel was that of an aluminum alloy having a rim size of 6JJX15. The tire inflation pressure was 200 kPa.

Here, the vertical force F_x means a force in the vertical direction (x-direction). The vertical force F_x is mainly its share of the vehicle weight and the reactive force from the ground. The lateral force F_y means a force in the lateral direction (y-direction). The lateral force F_y (side force) includes a cornering force. The longitudinal force F_z means a force in the back and forth direction (z-direction). The longitudinal force F_z may include a breaking force and accelerating force. In this case, the torque F_t means a force around a vertical axis perpendicular to the wheel axis CL (or around x-axis). The torque F_t may include a self-aligning torque and steer torque. The xyz directions are referred to in the orthogonal coordinate system fixed to the wheel as shown in Fig.3.

In each condition, typical values of the above-mentioned tire size were used for the various forces, and while applying such forces the strain was measured.

The expression "three-, six-, nine- and twelve-o'clock positions"

means the measuring positions P1-P4 around the rotational axis CL in the wheel plane as shown in Fig.3.

Incidentally, the unit " μ -strain" for the strain means 1×10^{-6} , namely, 0.0001 %.

In every condition, the compressive strain (-) occurs and becomes maximum at the six-o'clock position P1. In particular, the strain under the condition (2) (dashed line) becomes maximum in the four conditions.

At the twelve-o'clock position P3, on the other hand, a tensile strain (+) occurs in every condition.

Under such a condition that a torque F_t is applied as the condition (4) (chain double-dashed line), the difference of the strain from that under condition (1) becomes reversed between the three-o'clock position P4 and nine-o'clock position P3.

More, specifically, at the three-o'clock position P4 (rear in the traveling direction), the stress inclines towards the tension side although it inclines towards the compression side at the nine-o'clock position P2 (front in the traveling direction).

Under such a condition that a longitudinal force F_z is applied, at either the three-o'clock position P4 or nine-o'clock position P2, the strain shows a maximum towards the tensile side whereas it does not show any maximum at the other position.

For example, when a large braking force is exerted, the strain largely inclines towards the tensile side at the three-o'clock position as shown in Fig.2.

As explained above, the strain S varies depending on both the measuring position P and combination of various forces F exerted on the vehicle wheel 2. The strain S occurring on a wheel has sensibilities to the respective wheel forces F and the

sensibilities vary depending on the measuring position P , and the variations (curves in Fig.2) are generally different from each other as explained above.

When wheel forces F such as vertical force F_x , lateral force F_y , longitudinal force F_z and torque F_t are exerted on the vehicle wheel at the same time, the strain S at a certain position on the wheel disk is the summation of the strains caused by the respective wheel forces.

Thus, using the physical parameters (radial strains) measured at the predetermined specific positions P , the wheel forces can be obtained by solving simultaneous equations prepared in advance through measurements of the parameters at the above-mentioned predetermined positions P .

Taking the above-mentioned example where the physical parameters are radial strains and the predetermined specific positions are the six-o'clock, nine-o'clock, twelve-o'clock and three-o'clock positions P_1-P_4 , a method of making the simultaneous equations is explained below.

As the strain S at any position P is a function of the wheel forces F , the strain "Sa" at the six-o'clock position P_1 , the strain "Sb" at the twelve-o'clock position P_3 , the strain "Sc" at the three-o'clock position P_4 and the strain "Sd" at the nine-o'clock position P_2 can be expressed as follows:

$$Sa(F_x, F_y, F_z, F_t) = A_1 \times F_x + A_2 \times F_y + A_3 \times F_z + A_4 \times F_t$$

$$Sb(F_x, F_y, F_z, F_t) = B_1 \times F_x + B_2 \times F_y + B_3 \times F_z + B_4 \times F_t$$

$$Sc(F_x, F_y, F_z, F_t) = C_1 \times F_x + C_2 \times F_y + C_3 \times F_z + C_4 \times F_t$$

$$Sd(F_x, F_y, F_z, F_t) = D_1 \times F_x + D_2 \times F_y + D_3 \times F_z + D_4 \times F_t$$

wherein

A_1-A_4 , B_1-B_4 , C_1-C_4 and D_1-D_4 are coefficients corresponding to

the above-mentioned sensibilities of the strain to the respective wheel forces (F_x , F_y , F_z , F_t) at the respective position P . Incidentally, the sensibility is the ratio of the variation of the strain to the variation of the force.

Thus, the wheel force F can be obtained by computing equations, for example the following determinant.

$$\begin{bmatrix} F_x \\ F_y \\ F_z \\ F_t \end{bmatrix} = \begin{bmatrix} A1 & A2 & A3 & A4 \\ B1 & B2 & B3 & B4 \\ C1 & C2 & C3 & C4 \\ D1 & D2 & D3 & D4 \end{bmatrix}^{-1} \begin{bmatrix} Sa(F_x, F_y, F_z, F_t) \\ Sb(F_x, F_y, F_z, F_t) \\ Sc(F_x, F_y, F_z, F_t) \\ Sd(F_x, F_y, F_z, F_t) \end{bmatrix}$$

The above-mentioned coefficients $A1-A4$, $B1-B4$, $C1-C4$ and $D1-D4$ can be found as follows:

$$\begin{aligned} A1 &= \{Sa(500, 0, 0, 0) - Sa(0, 0, 0, 0)\}/500 \\ A2 &= \{Sa(500, 400, 0, 0) - Sa(500, 0, 0, 0)\}/400 \\ A3 &= \{Sa(500, 0, 400, 0) - Sa(500, 0, 0, 0)\}/400 \\ A4 &= \{Sa(500, 0, 0, 5) - Sa(500, 0, 0, 0)\}/5 \\ B1 &= \{Sb(500, 0, 0, 0) - sb(0, 0, 0, 0)\}/500 \\ B2 &= \{Sb(500, 400, 0, 0) - sb(500, 0, 0, 0)\}/400 \\ B3 &= \{Sb(500, 0, 400, 0) - sb(500, 0, 0, 0)\}/400 \\ B4 &= \{Sb(500, 0, 0, 5) - sb(500, 0, 0, 0)\}/5 \\ C1 &= \{Sc(500, 0, 0, 0) - sc(0, 0, 0, 0)\}/500 \\ C2 &= \{Sc(500, 400, 0, 0) - sc(500, 0, 0, 0)\}/400 \\ C3 &= \{Sc(500, 0, 400, 0) - sc(500, 0, 0, 0)\}/400 \\ C4 &= \{Sc(500, 0, 0, 5) - sc(500, 0, 0, 0)\}/5 \\ D1 &= \{Sd(500, 0, 0, 0) - sd(0, 0, 0, 0)\}/500 \\ D2 &= \{Sd(500, 400, 0, 0) - sd(500, 0, 0, 0)\}/400 \\ D3 &= \{Sd(500, 0, 400, 0) - sd(500, 0, 0, 0)\}/400 \\ D4 &= \{Sd(500, 0, 0, 5) - sd(500, 0, 0, 0)\}/5 \end{aligned}$$

For details, as to a group of the first four equations relating to the six-o'clock position P1: without applying any wheel force F , the strain $sa(0, 0, 0, 0)$ is measured. And by applying vertical force F_x of 500 kgf only, the strain $sa(500, 0, 0, 0)$ is measured. Further, by applying lateral force F_y of 400 kgf together with vertical force F_x of 500 kgf, the strain $sa(500, 400, 0, 0)$ is measured. Furthermore, by applying vertical force F_x of 500 kgf and torque F_t of 5 kgf·m, the strain $sa(500, 0, 0, 5)$ is measured. Then, by making the above calculation, the coefficients A1-A4 are obtained.

As to the remaining three groups, in the same way as above excepting the measuring positions P, the strains are measured and by making the calculation, the coefficients B1-B4, C1-C4 and D1-D4 can be obtained.

In the above-mentioned embodiment, in order to obtain four kinds of wheel forces, four measuring positions P1-P4 are necessitated. As understood from the above description, at least the same number of measuring positions as the number of the wheel forces are necessitated. Therefore, if only one kind of force, for example, the longitudinal force is required to control the undermentioned brake system BS, the number of the measuring position may be reduced to only one (three-o'clock position), but in order to promote accuracy, two or more positions are desired.

In order to measure the physical parameters, various detectors or sensors of mechanical type, semiconductor type etc. may be used. In this example, in view of the stability against temperature variation, a strain gauge of wire resistance type is used. But it is of course possible to use another type of sensor depending on the kind of the parameter and the environment.

As known from the above description, the device for determining the wheel force according to the present invention must be able to determine the physical parameters (strain S) of the rolling wheel $2b$ while the vehicle is traveling.

Fig.4 is a block diagram showing an example of the device which can output electronic data on all of the above-mentioned wheel forces on each wheel of a four-wheeled vehicle in order to, for example, provide: data on the longitudinal force F_z , especially, breaking force for the undermentioned brake system BS; data on the torque F_t for a steering system such as a steer-by-wire system SW which requires feedback when the driver turns the steering wheel; and data on the vertical force F_x and lateral force F_y for a suspension control system and attitude control system.

In this example, four strain gauge sensors 3A, 3B, 3C and 3D are provided on the wheel disk $2b2$ every 90 degrees around the rotational axis CL of the wheel $2b$ under the same conditions, e.g. at the same distance C from the rotational axis as shown in Fig.1. This is because the strain S can be measured at four positions P1-P4 without time lag. But, in case of a system which permits a slight time lag, the use of less sensors or only one sensor 3 may be possible because the sensor 3 can measure the force F at every position P while moving around the rotational axis CL.

In this example, as the sensors 3 are fixed to the wheel disk $2b2$, these are rotated together with the wheel. Therefore, to transmit the measured data, wireless transmission system is employed between the vehicle wheels 2 and the vehicle body, which comprises a transmitter TR on each wheel $2b$ and a receiver RE disposed on the vehicle body. The transmission system may

utilize radio waves, lightwave or electromagnetic induction.

As to the positions to which the sensor are fixed, in case of a combination of a tire and a wheel, the rim 2b1 is not preferable because the strain is liable to vary widely by other factors than wheel force, for example, tire inflation pressure, road surface conditions, tire engaging force and the like, and it is very difficult to discriminate the wheel forces. In contrast to the rim, the wheel disk 2b2 is generally easy to discriminate the wheel forces as explained above, but, in order to minimize the adverse effects of the relatively large rim deformation, a position in the direction of the hub or in the middle is generally preferred rather than the near rim position on the radius part 2b2.

As the sensors 3 are moved during the wheel is rotating, it is necessary to locate the sensors 3 with a sensor-locating device TG.

Fig.6 shows an example of the detector part of the sensor-locating device TG. In this example, the detector part comprises a magnetic material MG fixed to each wheel, a magnetic sensor MS provided on the vehicle body, and a pulse generator PG. The magnetic material MG and magnetic sensor MS constitute a part of a trigger device.

The trigger device outputs a trigger signal when the magnetic material MG gets near to the magnetic sensor MS. In this example, the magnetic material MG is one piece of magnet, and the trigger signal is outputted once per one revolution of the wheel.

The pulse generator PG outputs a pulse every predetermined rotational angle of the wheel. In this embodiment, the pulse

generator PG is a combination of a rotor provided with teeth at even intervals and disposed on the vehicle axle to rotate together with the vehicle wheel, and a generator outputting one pulse corresponding to each tooth detected.

If the pulse number per one revolution is for example 48 pulses, when 12 pulses are counted, starting with a trigger signal, the wheel has rotated 90 degrees.

Although another arrangement is possible, in this example, for the sake of simple explanation, the magnetic sensor MS and magnetic material MG are arranged such that, when the sensors 3A-3D are at the measuring positions P, namely, the above-mentioned three, six, nine and twelve-o'clock positions P1-P4, a trigger signal is generated.

More specifically, at the time the trigger signal is generated, the sensor 3A is at the six-o'clock position P1, the sensor 3B is at the nine-o'clock position P2, the sensor 3C is at the twelve-o'clock position P3 and the sensor 3D is at the three-o'clock position P4 as shown in Fig.1. Accordingly, when 12 pulses are counted, 3A is at P2, 3B at P3, 3C at P4 and 3D at P1. When 24 pulses are counted, 3A is at P3, 3B at P4, 3C at P1 and 3D at P2. When 36 pulses are counted, 3A is at P4, 3B at P1, 3C at P2 and 3D at P3. When 48 pulses are counted, the wheel made one revolution, and 3A is returns to P1, 3B to P2, 3C to P3 and 3D to P4. Therefore, the angle of rotation of the wheel from a reference position (namely, trigger signal generating position) is known from the count number, and the sensors can be easily located.

Aside from the above-mentioned combination of one magnetic sensor MS and one magnetic material MG per a wheel, a combination

of the single magnetic material MS and a plurality of magnetic sensors MS disposed on the vehicle body is also possible. In this case, using the sensors MS of the same number as that of the measuring positions P or more, the sensors 3 can be easily located without counting the pulses thus without using the pulse generator and counter.

The analog output of the sensor 3 is usually very small. Therefore, a linear amplifier AMP is used. But if the sensor output is nonlinear, a nonlinear or equalizer amplifier AMP is preferably used. if necessary, an analog to digital converter may be included in the amplifier AMP.

The outputs from the amplifiers AMP of the respective sensors 3A-3D are encoded/modulated and send out by the transmitter TR.

The transmitted signal is received and decoded/demodulated by the receiver RE, and outputted towards the controller CON comprising a CPU, memory, I/O device and the like.

The amplifier AMP and transmitter TR is fixed to the wheel, but it may be also possible to fix to another part as far as the part rotates together with the wheel such as a braking mechanism or near part.

In case of the construction shown in Fig.4 and the above-mentioned magnetic material MG and sensor MS arrangement, the following processes are carried out by the controller CON with respect to each wheel if the traveling direction is forward. If reverse, similar processes or other processes may be carried out. Incidentally, the controller CON can get the data on the traveling direction from a switch connected with the transmission selector or the like.

when the ignition switch of the vehicle is turned to ON and power is applied to the controller CON etc., as shown in Fig.5, the controller CON: waits for a trigger signal; if a trigger signal is detected, starts to count pulses; and the same time, checks if the count number reaches to the preset numbers (in this example, 12, 24, 36 and 48); if not, continues to count the pulses; if the count number is one of the preset numbers, locates the sensors by using the count number as explained above; and at the same time, checks if the count number is the maximum preset number (48), if so, resets the pulse counter to zero; after the sensors are located, fetches data on the strain at each measuring position from the sensor through the transmission system; and then computes the wheel forces by using the strain data and information such as the above-mentioned equations or determinant which has been acquired from the measurement of the wheel in advance and stored on the memory; and outputs electronic data of the required wheel force (in this example, all of the above-mentioned vertical force F_x , lateral force F_y , longitudinal force F_z and torque F_t) toward the computer-aided control systems BS, SW.

The existing anti lock brake system monitors the rotation of the wheel during braking, and controls the braking mechanism not to lock the wheel by reducing the force restraining the rotation of the wheel if wheel lock is detected. Thus, during locked, as the tire goes into a skid where the friction coefficient is very small, even if the locked time is very short, the frictional force becomes considerably decreased.

In the brake system BS according to the present invention, a controller monitors the longitudinal force F_z (breaking force)

during braking, and controls the braking mechanism BK so that the breaking force (frictional force) becomes maximum by reducing or increasing the force restraining the rotation of the wheel. Thus, the breaking distance becomes always minimized.

In the steer-by-wire system SW according to the present invention, a reactive force corresponding to or proportional to the torque F_t (self-aligning torque) is applied to the steering wheel of the vehicle as feedback by using a torque generator such as electric motor. Therefore, the driver's feel is remarkably improved.

Fig.7 shows another example of the detector part of the sensor-locating device TG which can locate the sensors 3 without counting the pulses from the pulse generator PG. In this example, the detector part comprises the magnetic material MS made up of a plurality of magnets, and a plurality of magnetic sensors MS1 and MS2. The magnets are grouped such that each group has a unique arrangement of the north pole (N) and south pole (S) so as to be able to identify the group by detecting the NS pole arrangement. The following is an example of the NS pole arrangement in case the group number is four and the pole number in each group is two

Group(Position)	NS pole arrangement
1	N + N
2	S + N
3	N + S
4	S + S

In this method, by increasing the number of NS poles in each group and the number of groups, the angularly resolution can be easily improved. Of course this concept can be applied to not only magnetism but also other physical properties as far as

sensible by appropriate sensing devices.

The electric power for the transmitter TR, amplifiers AMP, sensors 3 and so forth provided on the vehicle wheel may be supplied through a wireless system utilizing, for example, electromagnetic induction. But, in this example, the electric power is supplied through a power transmission unit utilizing physical contact between electric conductors such as slip ring unit. In this case, it is possible to use the physical contact type power transmission unit in order to send the sensor data from the wheels to the vehicle body. More specifically, the transmitter TR generates a carrier wave modulated by the sensor data and superposes the modulated carrier wave on the DC power. The modulated carrier wave is split off from the DC power and demodulated into the sensor data by the receiver RE.